

LAMINAR BOUNDARY LAYERS
Answers to problem sheet 2
Boundary layer equations

1. The 2d, incompressible boundary layer equations are derived in Chapter II (see page 8 of the notes). Starting with the 2d N-S equations, and using the given scaled values given for the variables u , v , P , x and y (same as in lecture notes, after we choose $\delta/L = Re^{-1/2}$), we get,

$$\begin{aligned} \frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} &= \\ u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} &= -\frac{\partial P'}{\partial x'} + \frac{1}{Re} \frac{\partial^2 u'}{\partial x'^2} + \frac{\partial^2 u'}{\partial y'^2} \\ \frac{1}{Re} \left\{ u' \frac{\partial v'}{\partial x'} + v' \frac{\partial v'}{\partial y'} \right\} &= -\frac{\partial P'}{\partial y'} + \frac{1}{Re} \left\{ \frac{1}{Re} \frac{\partial^2 v'}{\partial x'^2} + \frac{\partial^2 v'}{\partial y'^2} \right\}. \end{aligned}$$

In the limit $Re \rightarrow \infty$, we can neglect all the terms containing a factor $1/Re$ or smaller. Hence, we get the non-dimensional boundary layer equations,

$$\begin{aligned} \frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} &= 0 \\ u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} &= -\frac{\partial P'}{\partial x'} + \frac{\partial^2 u'}{\partial y'^2} \\ \frac{\partial P'}{\partial y'} &= 0. \end{aligned}$$

Boundary conditions:

1. No-slip on body surface at $y' = 0$, $u' = v' = 0$,
2. At the exterior edge, the velocity is given by the slipping velocity at the body surface given by inviscid theory, $u'_e(x')$, so

$$u' \rightarrow u'_e(x').$$

2. Integral Momentum Equation:

By integrating the momentum equation through the boundary layer, we have,

$$\begin{aligned} \int_0^\infty \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) dy &= \int_0^\infty \left(u_e \frac{du_e}{dx} + \nu \frac{\partial^2 u}{\partial y^2} \right) dy \\ \text{i.e. } \int_0^\infty \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - u_e \frac{du_e}{dx} \right) dy &= \nu \left[\frac{\partial u}{\partial y} \right]_0^\infty. \end{aligned}$$

When $y \rightarrow \infty$, $u \rightarrow u_e(x)$ which is independent of y so,

$$\left(\frac{\partial u}{\partial y} \right)_{y=\infty} = 0.$$

Hence,

$$\int_0^\infty \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - u_e \frac{du_e}{dx} \right) dy = -\nu \left(\frac{\partial u}{\partial y} \right)_{y=0}.$$

Using the usual boundary layer scaling,

$$u' = \frac{u}{U}, \quad v' = \frac{v}{U} Re^{1/2}, \quad u'_e = \frac{u_e}{U}, \quad x' = \frac{x}{L}, \quad y' = \frac{y}{L} Re^{1/2}, \quad \text{with } Re = \frac{UL}{\nu},$$

we get,

$$\int_0^\infty \left(u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} - u'_e \frac{du'_e}{dx'} \right) dy' = - \left(\frac{\partial u'}{\partial y'} \right)_{y'=0} = \frac{1}{2} c_f Re^{1/2}.$$

We have defined the skin friction coefficient as

$$\frac{1}{2} c_f Re^{1/2} = \left(\frac{\partial u'}{\partial y'} \right)_{y'=0}.$$

The left hand-side of the integral momentum equation can be re-written as,

$$\int_0^\infty \left(u' \frac{\partial u'}{\partial x'} + \frac{\partial}{\partial y'} (u'v') - u' \frac{\partial v'}{\partial y'} - u'_e \frac{du'_e}{dx'} \right) dy',$$

and the continuity equation gives,

$$\frac{\partial v'}{\partial y'} = -\frac{\partial u'}{\partial x'},$$

so we get,

$$\int_0^\infty \left(2u' \frac{\partial u'}{\partial x'} - u'_e \frac{du'_e}{dx'} \right) dy' + [u'v']_0^\infty = -\frac{1}{2} c_f Re^{1/2}.$$

We can simplify the left hand-side term by writing,

$$\begin{aligned} 2u' \frac{\partial u'}{\partial x'} &= \frac{\partial}{\partial x'} (u'^2) \\ \text{and } [u'v']_0^\infty &= \left[-u' \int_0^{y'} \frac{\partial u'}{\partial x'} dy' \right]_0^\infty \\ &= -u'_e \int_0^\infty \frac{\partial u'}{\partial x'} dy'. \end{aligned}$$

Hence, the integral momentum equation becomes,

$$\begin{aligned} \int_0^\infty \left(-\frac{\partial}{\partial x'} (u'^2) + u'_e \frac{du'_e}{dx'} \right) dy' + u'_e \int_0^\infty \frac{\partial u'}{\partial x'} dy' &= \frac{1}{2} c_f Re^{1/2} \\ \text{i.e. } \int_0^\infty \left(\frac{\partial}{\partial x'} (u'(u'_e - u')) \right) dy' + \frac{du'_e}{dx'} \int_0^\infty (u'_e - u') dy' &= \frac{1}{2} c_f Re^{1/2}. \end{aligned}$$

The momentum and displacement thicknesses are defined as,

$$\begin{aligned} \theta &= \int_0^\infty \frac{u'}{u'_e} \left(1 - \frac{u'}{u'_e} \right) dy' \\ \delta^* &= \int_0^\infty \left(1 - \frac{u'}{u'_e} \right) dy'. \end{aligned}$$

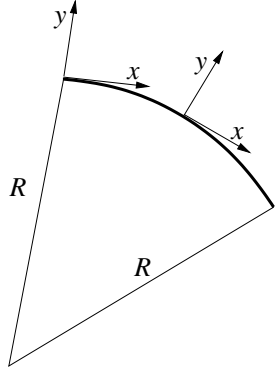
By substituting these expressions into the integral momentum equation, we finally get

$$\frac{1}{2}c_f Re^{1/2} = \frac{d}{dx'} (u_c'^2 \theta) + \delta^* u_c' \frac{du_c'}{dx'}$$

3. For the flow on a plane surface, the two-dimensional boundary layer equations give

$$\frac{\partial P}{\partial y} = 0,$$

so that the pressure is constant through the boundary layer.



This is not strictly true for the flow over a curved surface. We adopt curvilinear coordinates, where x is taken along the surface in the direction of the flow, and y is normal to the flow (see sketch). In this case, a pressure gradient normal to the wall is required to balance the centrifugal forces associated with the curved flow, so we have

$$\frac{\partial P}{\partial y} = \rho \frac{u^2}{R},$$

where R is the radius of curvature of the surface.

In dimensional terms, we get

$$\Delta P \sim O(\rho \frac{U^2}{R} \delta),$$

where δ is the thickness of the boundary layer at a given x , and U the velocity scale for the x -direction. The latter expression can be rewritten in non-dimensional terms as

$$\frac{\Delta P}{\rho U^2} \sim O(\frac{\delta}{R}).$$

Hence, the pressure gradient through the boundary layer can be neglected if

$$\frac{\delta}{R} \ll 1.$$

4. The exact solution to the equation is

$$w = A + Be^{-x/\epsilon},$$

and the boundary conditions give

$$1 = A + B, \quad 2 = A + Be^{-1/\epsilon},$$

i.e.

$$B = \frac{1}{e^{-1/\epsilon} - 1}, \quad A = 1 - \frac{1}{e^{-1/\epsilon} - 1} = \frac{e^{-1/\epsilon} - 2}{e^{-1/\epsilon} - 1}.$$

Hence,

$$w = \frac{1}{e^{-1/\epsilon} - 1} (e^{-1/\epsilon} - 2 + e^{-x/\epsilon}).$$

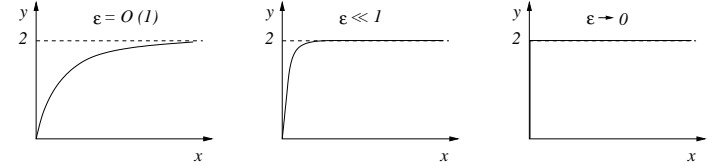
(1) For $x/\epsilon = X = O(1)$, since $0 < \epsilon \ll 1$, $e^{-1/\epsilon} \sim 0$, and hence,

$$w \sim 2 - e^{-X}.$$

(2) For $x/\epsilon \gg 1$,

$$w \sim -(-2) = 2.$$

The solution exhibits a rapid variation near $x = 0$, *i.e.* a boundary layer. The thickness of the boundary layer is $O(\epsilon)$ (see sketch).



The problem can be solved using matched expansions.

• Outer region:

$$w = w_0 + \epsilon w_1 + \dots \Rightarrow \epsilon(w_0'' + \epsilon w_1'' + \dots) + (w_0' + \epsilon w_1' + \dots) = 0$$

To leading order, $w_0' = 0$ so $w_0 = A$. The above discussion, suggests BL at $x = 0$, so in the outer region, apply the boundary condition at $x = 1 \Rightarrow A = 2$.

• Inner region:

$$w = w_0 + \epsilon w_1 + \dots \quad \text{and} \quad x = \epsilon X,$$

since there is a boundary layer of thickness ϵ . Hence we get at leading order,

$$w_0'' + w_0' = 0,$$

with solution $w_0 = C + De^{-X}$. The boundary condition at $x = 0$ gives $C + D = 1 \Rightarrow w_0 = C + (1 - C)e^{-X}$. Matching as $X \rightarrow \infty$ yields $C = 2$, *i.e.*

$$w_0 = 2 - e^{-X}.$$

These results are the same as obtained by direct solution of the equation.