

Three hours

THE UNIVERSITY OF MANCHESTER

CONTINUUM MECHANICS

24 January 2017

09:45 – 12:45

Answer **ALL THREE** questions in section A (21 marks in total).

Answer **THREE** of the **FOUR** questions in section B (54 marks in total). If more than **THREE** questions from Section B are attempted, then credit will be given for the best **THREE** answers.

University approved calculators may be used.

SECTION A

A1. Newton's law for a particle can be written as $\mathbf{F} = m\mathbf{A}$, where \mathbf{F} is the resultant force, m is the mass of the particle and \mathbf{A} is the acceleration.

- (i) Define what is meant by an objective quantity.
- (ii) By direct differentiation of the position explain why Newton's second law for a particle is **not** objective.

[5 marks]

A2. Small particles are advected by a moving continuum, where $N(\mathbf{R}, t)$ denotes the number of particles per unit volume, \mathbf{R} is the Eulerian position and t is time.

- (i) If the total number of particles within a material region Ω_t is conserved, show that this condition is described by the equation

$$\frac{\partial N}{\partial t} + \nabla_{\mathbf{R}} \cdot (N\mathbf{V}) = 0,$$

where \mathbf{V} is the velocity of the continuum.

- (ii) Derive the modified conservation equation when there is a source of particles, $S(\mathbf{R}, t)$, within the continuum. Be sure to specify the units of S carefully.

[6 marks]

A3. Consider a sphere of solid material, initially of unit radius, that is first uniformly dilated into a sphere of radius r_1 and subsequently to a sphere of radius r_2 . You may assume a linear stretch: the deformed radius $R = \lambda r$, where λ is a constant to be determined for each deformation. A standard spherical polar coordinate system $(\xi^1, \xi^2, \xi^3) \equiv (r, \theta, \phi)$ is defined with origin at the centre of the undeformed sphere, such that the undeformed position is given by

$$\mathbf{r} = r \sin \theta \cos \phi \mathbf{e}_X + r \sin \theta \sin \phi \mathbf{e}_Y + r \cos \theta \mathbf{e}_Z,$$

where \mathbf{e}_X , \mathbf{e}_Y and \mathbf{e}_Z are unit vectors in a global Cartesian coordinate system.

- (i) Find the Green–Lagrange strain tensor associated with the first deformation, $\gamma_{ij}^{(1)}$.
- (ii) Find the Green–Lagrange strain tensor associated with the subsequent (second) deformation, $\gamma_{ij}^{(2)}$, assuming that the reference configuration is the state after the first deformation.
- (iii) Find the strain tensor associated with the total deformation from initial configuration to final configuration, γ_{ij} .
- (iv) Find a relationship between the three strain tensors, γ_{ij} , $\gamma_{ij}^{(1)}$ and $\gamma_{ij}^{(2)}$.

[10 marks]

SECTION B

B4. An incompressible material has the constitutive relationship

$$\mathbf{T} = -P\mathbf{I} + \eta_s \mathbf{D} + \hat{\mathbf{T}},$$

where P is the pressure, η_s is a constant and $\hat{\mathbf{T}}$ satisfies

$$\hat{\mathbf{T}} + \lambda_1 \hat{\mathbf{T}}^\nabla + \alpha \frac{\lambda_1}{\eta_p} \hat{\mathbf{T}}^2 = \eta_p \mathbf{D},$$

where η_p , λ_1 and α are constants. The upper-convected derivative is defined by

$$\mathbf{A}^\nabla = \frac{D\mathbf{A}}{Dt} - \mathbf{L}\mathbf{A} - \mathbf{A}\mathbf{L}^T,$$

where $\mathbf{L} = \nabla_{\mathbf{r}} \otimes \mathbf{V}$ is the Eulerian velocity gradient tensor and \mathbf{D} is the symmetric part of \mathbf{L} .

(i) Confirm that the constitutive relationships are objective.

You may assume that the Cauchy stress \mathbf{T} is objective; that the deformation gradient tensor, \mathbf{F} , transforms as $\mathbf{F}^* = \mathbf{Q}\mathbf{F}$, where \mathbf{Q} is an orthogonal matrix that expresses the relative rotation between observers; and that $\mathbf{L} = \dot{\mathbf{F}}\mathbf{F}^{-1}$.

A steady two-dimensional extensional flow is given by $\mathbf{V} = (\epsilon X, -\epsilon Y)$, where ϵ is a constant rate of extension and X and Y are Cartesian coordinates.

- (ii) Assuming now that $\hat{\mathbf{T}}$ is constant in time and space, find the Cartesian components of $\hat{\mathbf{T}}$ in this flow. Comment on any choice of roots. (You may assume that $1 + (\alpha\lambda_1/\eta_p)(\hat{T}_{XX} + \hat{T}_{YY}) \neq 0$.)
- (iii) Comment on the validity of the constitutive model by considering what happens to the stress component \hat{T}_{XX} as $\epsilon \rightarrow 1/(2\lambda_1)$ in the cases when $\alpha \neq 0$ and $\alpha = 0$.

[18 marks]

B5. Consider a hyperelastic solid that also undergoes isotropic growth.

- (i) If M is the rate of change of mass per unit deformed volume show by using the integral mass balance that the Eulerian form of the statement of conservation of mass is

$$\frac{D\rho}{Dt} + \rho \nabla_{\mathbf{R}} \cdot \mathbf{V} = M.$$

- (ii) Show that

$$\frac{D}{Dt} \int_{\Omega_t} \rho \phi \, dV_t = \int_{\Omega_t} \left(\rho \frac{D\phi}{Dt} + M\phi \right) dV_t,$$

where ϕ is a scalar field and Ω_t is a material volume. Hence show that the balance of linear momentum equation is unchanged in the presence of growth, under the assumption that the additional momentum due to growth is $M\mathbf{V}$ per unit deformed volume. Interpret this assumption.

- (iii) Growth can be modelled by assuming that the undeformed metric tensor (in a Cartesian coordinate system) is

$$g_{IJ} = \lambda_g^2(t) \delta_{IJ},$$

where $\lambda_g(t)$ is a function only of time that is related to the growth. The growing material is subject to a uniaxial extension such that

$$X_1 = \lambda_1 x_1, \quad X_2 = \lambda_2 x_2, \quad X_3 = \lambda_2 x_3.$$

Find G'_{ij} and hence find the values of λ_1 and λ_2 such that the Green–Lagrange strain tensor is zero.

B6. For an ideal gas the internal energy, Φ , Cauchy stress, \mathbb{T} , and entropy, η , depend only on the density, ρ , and temperature, Θ :

$$\Phi(\rho, \Theta), \quad \mathbb{T}(\rho, \Theta), \quad \eta(\rho, \Theta).$$

- (i) Use the fact that these quantities must remain indifferent under a change in Eulerian observer given by $\mathbf{R}^* = \mathbf{Q}(t)\mathbf{R}$ to deduce that

$$\mathbb{T} = -P(\rho, \Theta)\mathbf{I}, \tag{1}$$

where P is called the thermodynamic pressure and \mathbf{I} is the identity tensor.

- (ii) Use the Clausius–Duhem inequality in the absence of heat flux, together with conservation of mass to show that

$$P = \rho^2 \frac{\partial \Phi}{\partial \rho} - \rho^2 \Theta \frac{\partial \eta}{\partial \rho}, \quad \frac{\partial \Phi}{\partial \Theta} = \Theta \frac{\partial \eta}{\partial \Theta}.$$

- (iii) Show that the ideal gas constitutive laws

$$\Phi = c_v \Theta, \quad P = \rho R \Theta,$$

satisfy the equations deduced in (ii) provided that η has a particular form, which is to be found. Here c_v is a constant, the specific heat of the gas at constant volume, and R is the ideal gas constant.

[18 marks]

B7. An incompressible, hyperelastic solid cylinder has undeformed radius 1 and undeformed length 2. The cylinder undergoes a deformation such that it remains cylindrical with no twist and the deformed position is given by $R(r)$, $\Theta = \theta$ and $Z(z)$. The strain energy function of the solid material is given by

$$\mathcal{W} = C_1(I_1 - 3)^n + C_2(I_2 - 3)^m,$$

where m , n , C_1 and C_2 are constants.

- (i) Write down the deformed position in components in a global Cartesian coordinate system as a function of the undeformed cylindrical polar coordinates (r, θ, z) .
- (ii) Hence, compute the three strain invariants corresponding to this deformation.
- (iii) Use the incompressibility constraint to deduce the most general forms of R and Z and find corresponding values of the strain invariants.
- (iv) Compute the stress tensor T^{ij} in the deformed solid and confirm that Cauchy's equations are satisfied in the absence of body forces and accelerations.

Hint: In cylindrical polar coordinates $(\xi^1, \xi^2, \xi^3) = (r, \theta, z)$ the only non-zero Christoffel symbols are given by

$$\Gamma_{12}^2 = \Gamma_{21}^2 = \frac{1}{r} \quad \text{and} \quad \Gamma_{22}^1 = -r.$$

[18 marks]

FORMULA SHEET

- For a general (Lagrangian) coordinate system ξ^i :

$$\mathbf{g}_i = \frac{\partial \mathbf{r}}{\partial \xi^i}, \quad \mathbf{g}_i \cdot \mathbf{g}^j = \delta_i^j, \quad g_{ij} = \mathbf{g}_i \cdot \mathbf{g}_j, \quad g = \det(g_{ij}).$$

$$\mathbf{G}_i = \frac{\partial \mathbf{R}}{\partial \xi^i}, \quad \mathbf{G}_i \cdot \mathbf{G}^j = \delta_i^j, \quad G_{ij} = \mathbf{G}_i \cdot \mathbf{G}_j, \quad G = \det(G_{ij}).$$

- For a scalar field $f(\mathbf{x})$ and vector field $\mathbf{u}(\mathbf{x})$

$$\nabla f = \mathbf{g}^i \frac{\partial f}{\partial \xi^i}, \quad \operatorname{div} \mathbf{u} = \frac{1}{\sqrt{g}} \frac{\partial (u^i \sqrt{g})}{\partial \xi^i}, \quad \operatorname{curl} \mathbf{u} = \epsilon^{ijk} u_j |_{;i} \mathbf{g}_k.$$

- The material derivative in general coordinates is

$$\frac{DU^i}{Dt} = \frac{\partial U^i}{\partial t} + V^j U^i |_{;j},$$

where \mathbf{V} is the velocity of the continuum.

- Cauchy's equation in the usual notation in components in general coordinates ξ^i is

$$T^{ji} |_{;j} + \rho F^i = \rho \ddot{U}^i = \rho \frac{DV^i}{Dt}, \quad \text{where} \quad T^{ji} |_{;j} = T^{ji}_{;j} + \Gamma_{jr}^j T^{ri} + \Gamma_{jr}^i T^{jr},$$

and Γ_{jk}^i are the Christoffel symbols for the chosen coordinate system in the deformed configuration.

- The material derivative of the determinant of the deformation gradient tensor is

$$\frac{DJ}{Dt} = J \nabla_{\mathbf{R}} \cdot \mathbf{V}.$$

- The Reynolds Transport theorem states that

$$\frac{d}{dt} \int_{\Omega_t} \phi \, d\mathcal{V}_t = \int_{\Omega_t} \left(\frac{D\phi}{Dt} + \phi \nabla_{\mathbf{R}} \cdot \mathbf{V} \right) d\mathcal{V}_t,$$

where Ω_t is a material volume, ϕ is a scalar field and \mathbf{V} is the velocity of the continuum.

- For a Cartesian line element dX_I in the deformed configuration

$$\frac{DdX_I}{Dt} = V_{I,K} dX_K,$$

where V_I is the I -th Cartesian component of the velocity.

- Nanson's relation states that

$$dA_{\bar{i}} = J \frac{\partial \xi^j}{\partial \chi^{\bar{i}}} da_j,$$

where ξ^j are the Lagrangian coordinates, $\chi^{\bar{i}}$ are the Eulerian coordinates, J is the determinant of the deformation gradient tensor, $d\mathbf{A}$ is an area element in the deformed configuration and $d\mathbf{a}$ is an area element in the undeformed configuration.

- The Green–Lagrange strain tensor is defined by

$$\gamma_{ij} = \frac{1}{2} (G_{ij} - g_{ij}).$$

- The strain invariants are defined by

$$I_1 = g^{ij}G_{ji}, \quad I_2 = \frac{1}{2} (I_1^2 - g^{ir}g^{js}G_{ij}G_{rs}), \quad I_3 = G/g,$$

where $g = \det(g_{ij})$ and $G = \det(G_{ij})$

- A hyperelastic material is described by a strain energy function $\mathcal{W}(I_1, I_2, I_3)$ such that

$$T^{ij} = PG^{ij} + Ag^{ij} + BB^{ij},$$

where

$$A = \frac{2}{\sqrt{I_3}} \frac{\partial \mathcal{W}}{\partial I_1}, \quad B = \frac{2}{\sqrt{I_3}} \frac{\partial \mathcal{W}}{\partial I_2}, \quad P = 2\sqrt{I_3} \frac{\partial \mathcal{W}}{\partial I_3},$$

and $B^{ij} = [I_1 g^{ij} - g^{ir}g^{js}G_{rs}]$.

- The physical components of the stress tensor are given by $\sigma_{(ij)} = T^{ij} \sqrt{G_{jj}/G^{ii}}$ (no summation).
- The body stress tensor T^{ij} and second Piola–Kirchhoff stress tensor s^{ij} are related by the expression $JT^{ij} = s^{ij}$.
- The Clausius–Duhem inequality is

$$-\rho \dot{\Psi} - \rho \eta \dot{\Theta} - \frac{1}{\Theta} \mathbf{Q} \cdot \nabla_{\mathbf{R}} \Theta + \mathbb{T} : \mathbb{D} \geq 0,$$

where $\Psi = \Phi - \eta \Theta$.

- The most general transformation of position and time between observers in Euclidean space is

$$\mathbf{R}^*(t^*) = \mathbf{Q}(t) \mathbf{R}(t) + \mathbf{C}(t), \quad t^* = t - a,$$

where \mathbf{Q} is an orthogonal matrix, \mathbf{C} is a translation vector and a is a constant time shift.

END OF EXAMINATION PAPER